

# Metode Preloading

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# Metode Stabilisasi Tanah

## ◎ Soil Stabilization Techniques

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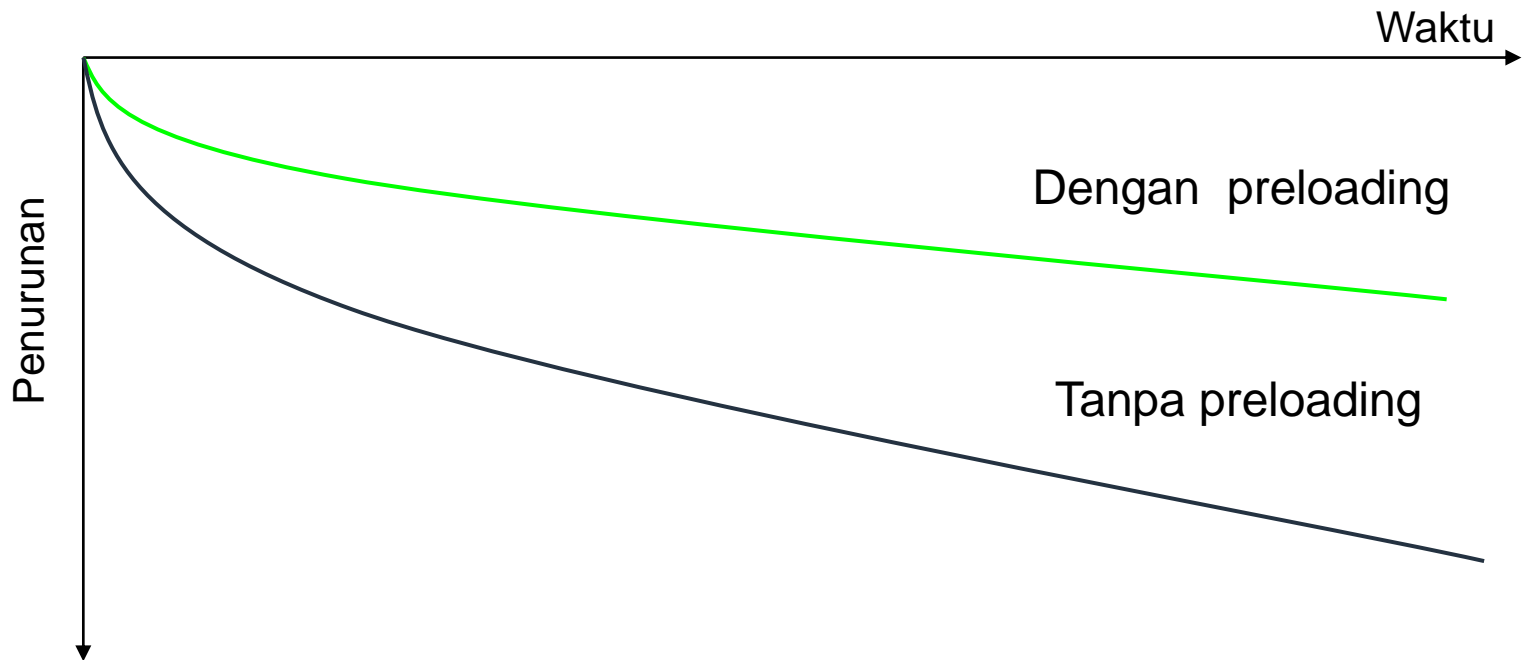
- > Mechanical (Shallow Compaction, Deep Compaction)
- > Hydraulic Modification (Drainage, Dewatering, **Preloading and Use of Vertical Drains**, Electronic Dewatering and Stabilization)
- > Physical and Chemical Modification (Use of Admixtures, Grouting, Thermal modification)
- > Modification by Inclusion and Confinement (Soil Reinforcement)

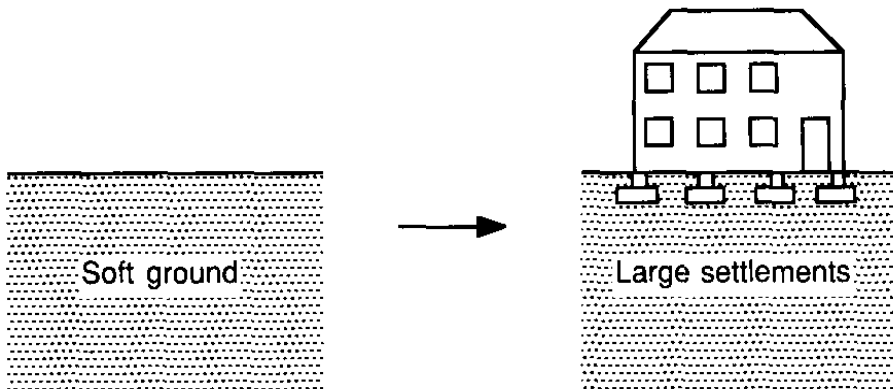
Ref: Hausman M.R (1990) Engineering Principles of Ground Improvement, Mc-Graw Hill.

# PRELOADING (PEMBEBANAN AWAL)

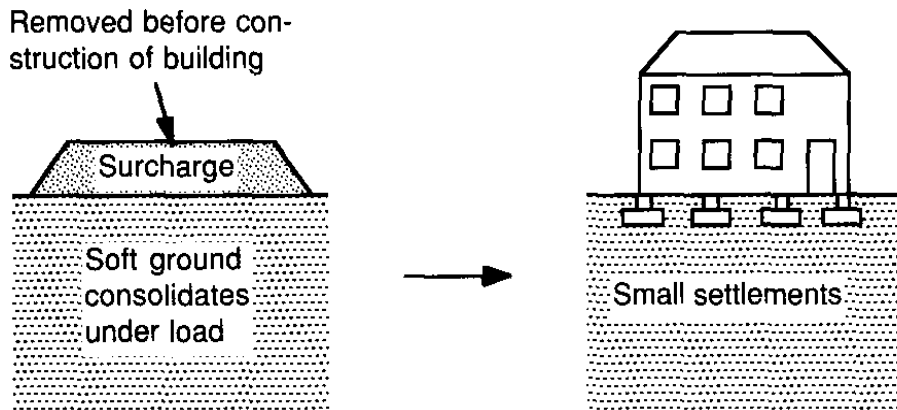
Mengurangi Penurunan:

- Pondasi di atas tanah lunak
- Beban yang diberikan  $>$  tekanan pra-konsolidasi ( $\sigma'_{o} + \Delta\sigma > \sigma'_c$ )

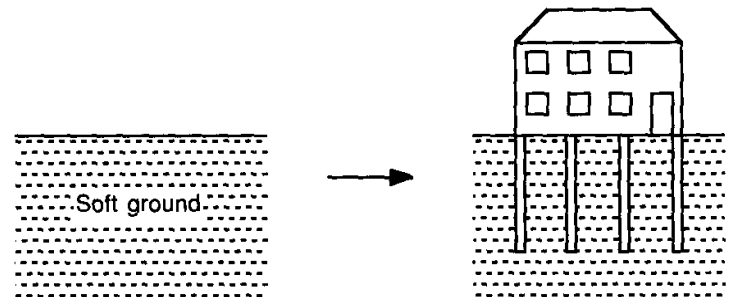




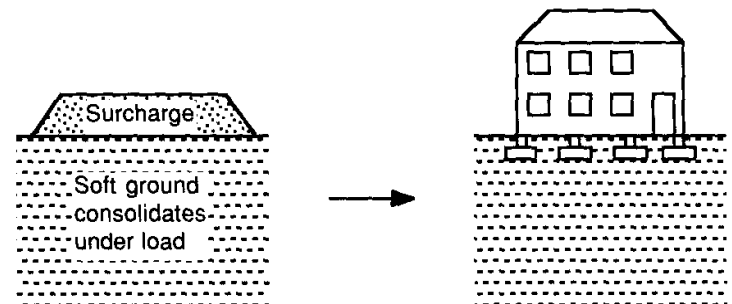
Soft ground causes large settlements



Preloading reduces settlements



Soft ground requires pile foundations



Preloading allows cheaper spread footings

b. Preloading may allow savings in foundation costs

# Assessment of Ground Conditions

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## Data yang diperlukan

- ✓ Stratifikasi tanah
- ✓ Kondisi aliran air dalam tanah (satu arah / dua arah)
- ✓ Koefisien Konsolidasi dan permeabilitas ( $C_v$ ,  $k_v$ )
- ✓ Sejarah pembebanan ( $\sigma'_c$ )

# Pertimbangan Perencanaan

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The criteria of settlement after construction,  
e.g.: *maximum total settlement of 25 mm (1") and differential settlement of 10 mm (0.4"), within a period of 6 month after construction*

Bearing capacity or shear strength of foundation soil (in term of maximum height of embankment)

Time available

$$H_{cr} = \frac{c_u Nc}{\gamma_f FS}$$

# JENIS PRELOADING

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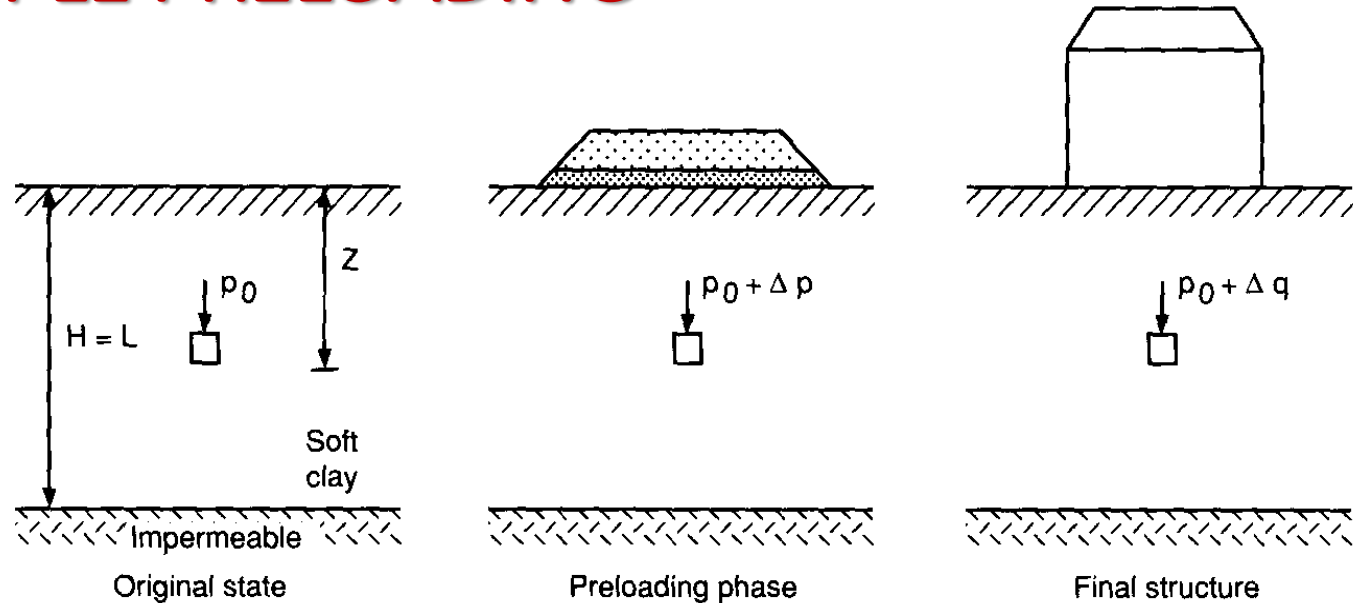
Simple Preloading

Surcharge Preloading

Staged Loading

Preloading with Vertical drain

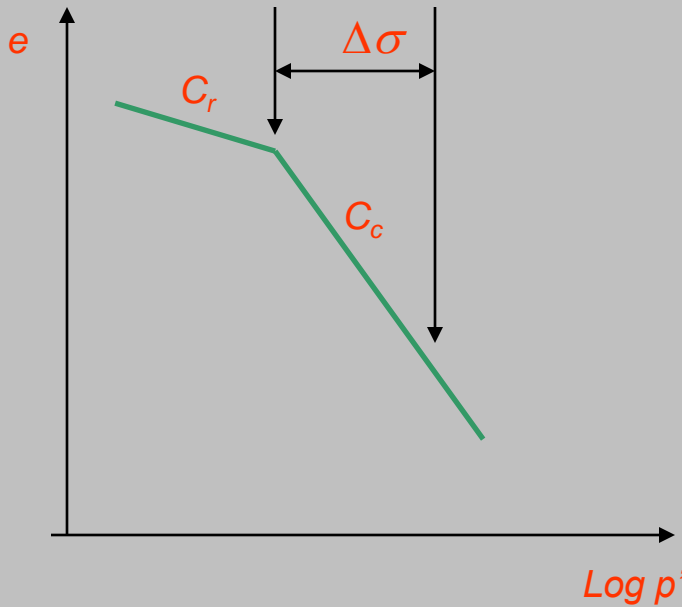
# SIMPLE PRELOADING



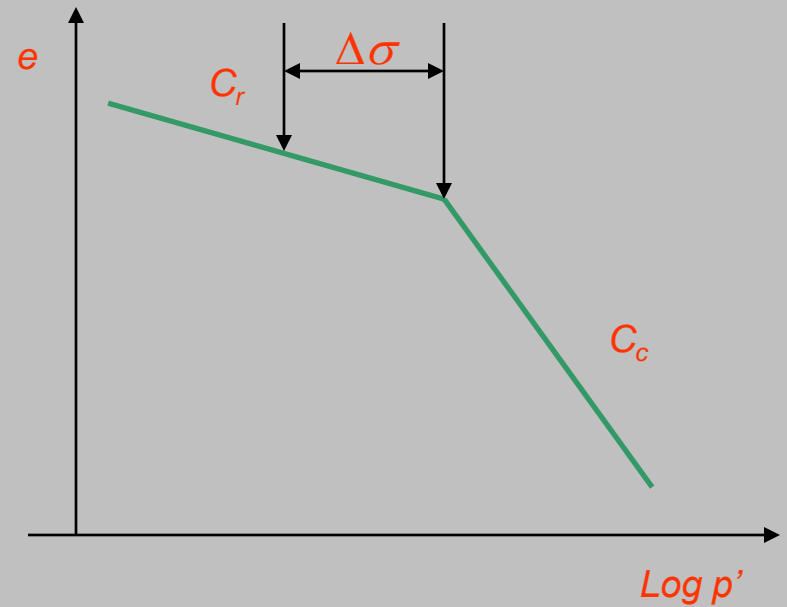
a. Simple preloading of a building site

- A surcharge equal to a future site load is applied ( $\Delta p = \Delta q$ )
- When consolidation of the foundation soil is reaching **90%** complete, then the surcharge is removed and the new building is erected





$$S_c = C_c \frac{H}{1 + e_o} \log \frac{\sigma_o + \Delta\sigma}{\sigma_o}$$



$$S_c = C_r \frac{H}{1 + e_o} \log \frac{\sigma_o + \Delta\sigma}{\sigma_o}$$

$$S_c = C_r \frac{H}{1 + e_o} \log \frac{\sigma_c}{\sigma_o} + C_c \frac{H}{1 + e_{o1}} \log \frac{\sigma_o + \Delta\sigma}{\sigma_c}$$

# Perhitungan penurunan tanah

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Final settlement due to surcharge:

$$S_{sf} = C_c \frac{H}{1 + e_o} \log \frac{\sigma_o + \Delta p}{\sigma_o}$$

Final settlement of the building:

$$S_{bf} = C_r \frac{H}{1 + e_o} \log \frac{\sigma_o + \Delta q}{\sigma_o}$$

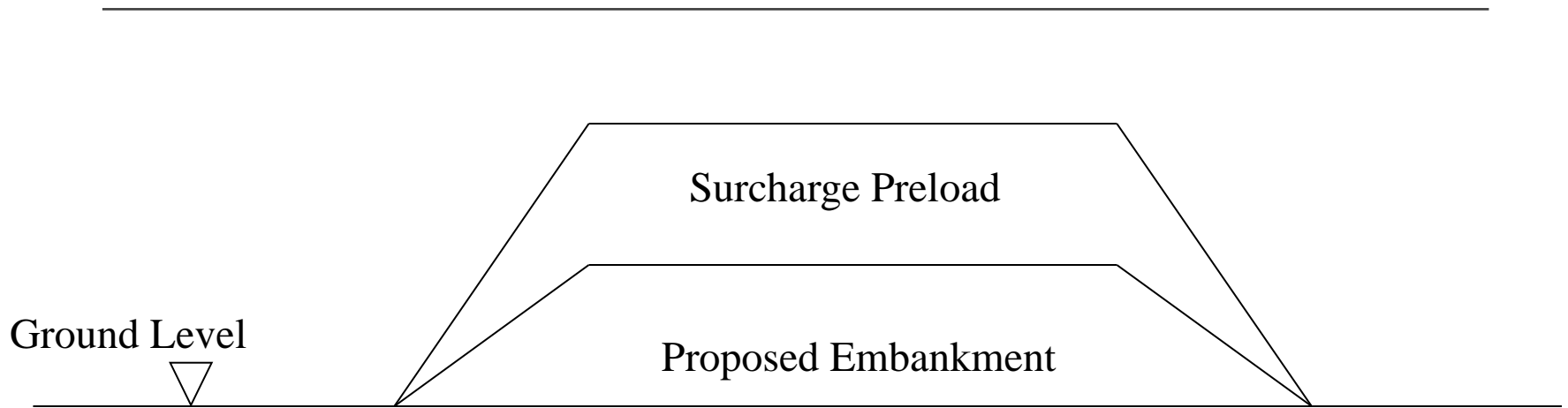
→ Less settlement (in order of 1 tenth)

**$C_c$  vs.  $C_r$  typical values:  $C_c = 0.1 - 0.8$   
 $C_r/C_c = 0.1 - 0.2$**

<b>Empirical formula</b>	<b>Soil type</b>
$C_c = 0.009 (LL - 10)$	All clay (undisturbed)
$C_c = 0.007 (LL - 10)$	Remolded soil
$C_c = 1.15 (e_o - 0.35)$	All clay (undisturbed)
$C_c = 0.30 (e_o - 0.27)$	An organic soil
$C_c = 1.15 \times 10^{-2} \omega_n$	Organic soil
$C_c = 0.75 (e_o - 0.50)$	Low plasticity soil
$C_c = G_s \frac{PI}{200}$	Wroth & Wood (1978)

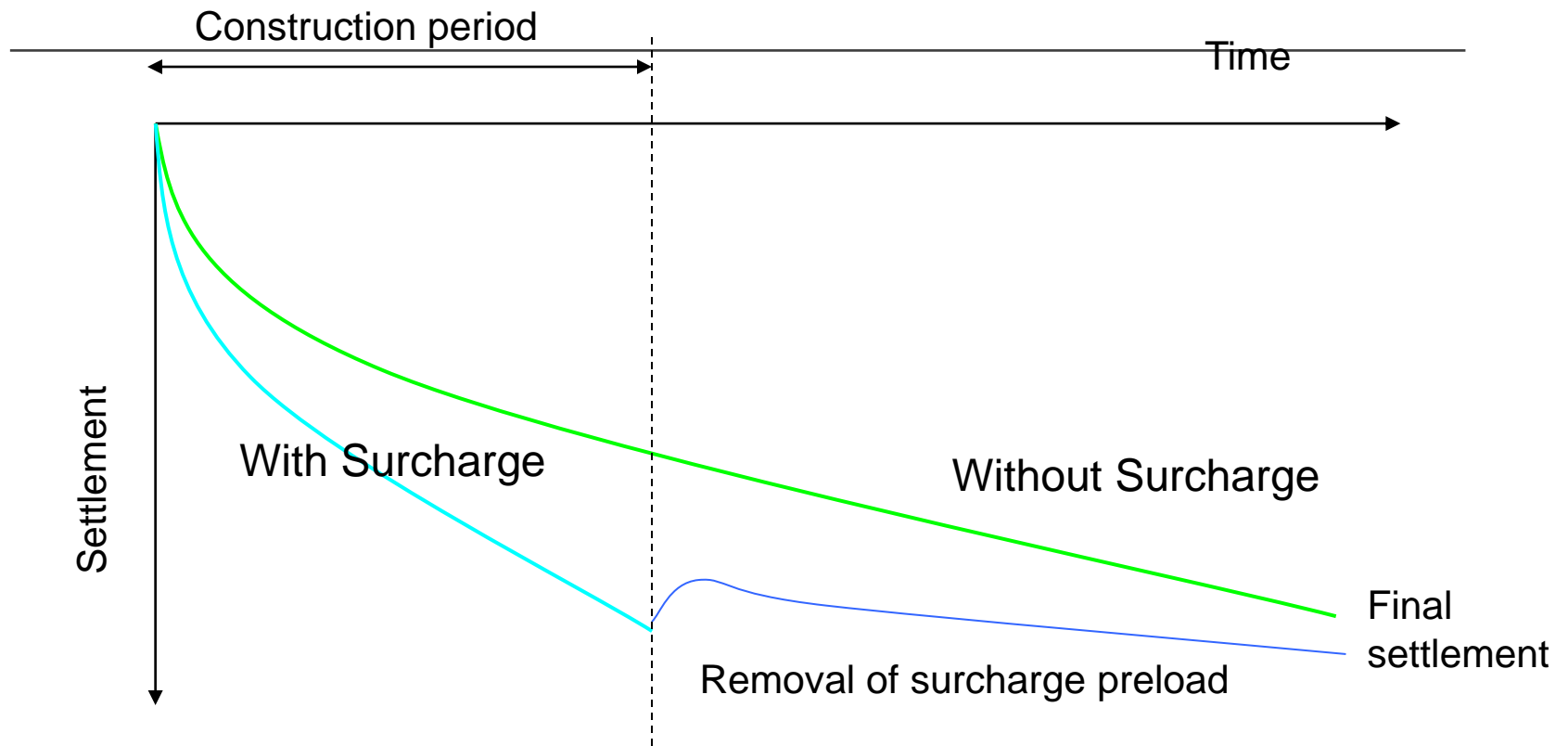
There are other relationships in textbooks

# SURCHARGE PRELOADING

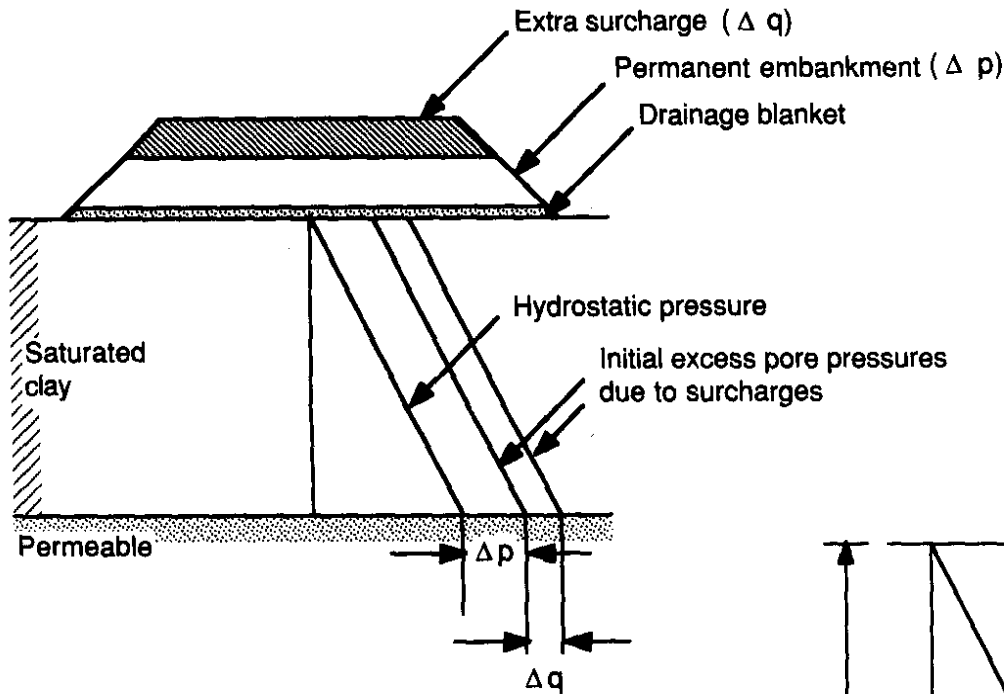


A permanent load ( $\Delta p$ ) + surcharge ( $\Delta q$ ) is placed, then after a certain period of time surcharge is removed

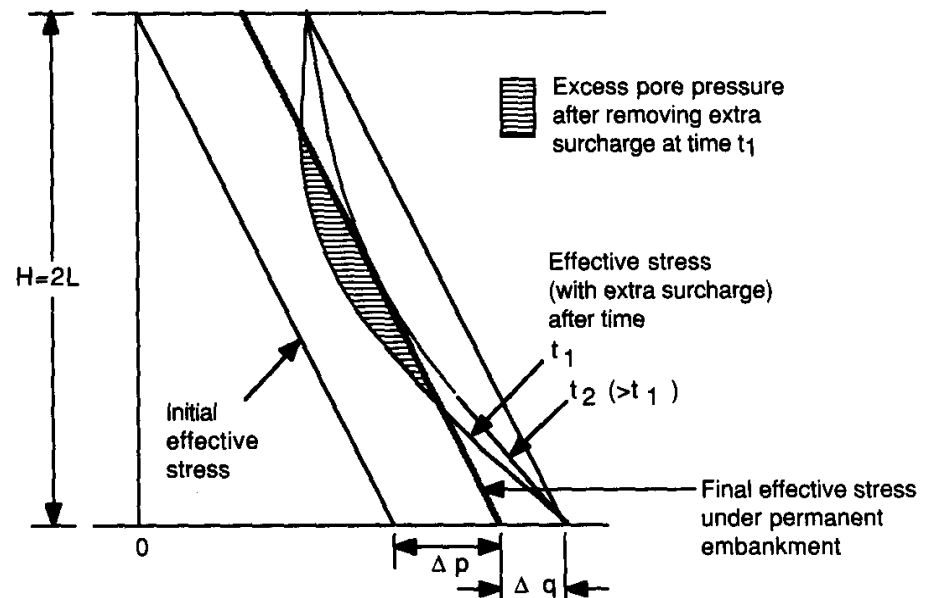
# Effect of Surcharge on Final Settlement



# Effect of surcharge on excess pwp



a. Initial pore pressures



In this sketch:  
 at time  $t_1$  :  $U(\text{avg.}) \cong 61\%$ ,  $T = 0.3$   
 at time  $t_2$  :  $U(\text{avg.}) \cong 76\%$ ,  $T = 0.5$

b. Effective stresses

# Rate of Consolidation

Settlement at time  $t$

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$$S_t = U_v S_f$$

$U_v$  = degree of consolidation (vertical direction) which can be correlated with the time factor  $T_v$

$$T_v = \frac{C_v t}{H_d^2}$$

$$U_v < 60\% \rightarrow T_v = (\pi/4) U^2$$

$$U_v > 60\% \rightarrow T_v = -0.933 \log(1-U) - 0.085 \\ = 1.781 - 0.933 \log(100\% - U\%)$$

$t$  = time (sec)

$C_v$  = coefficient of vertical consolidation ( $\text{m}^2/\text{sec}$ )

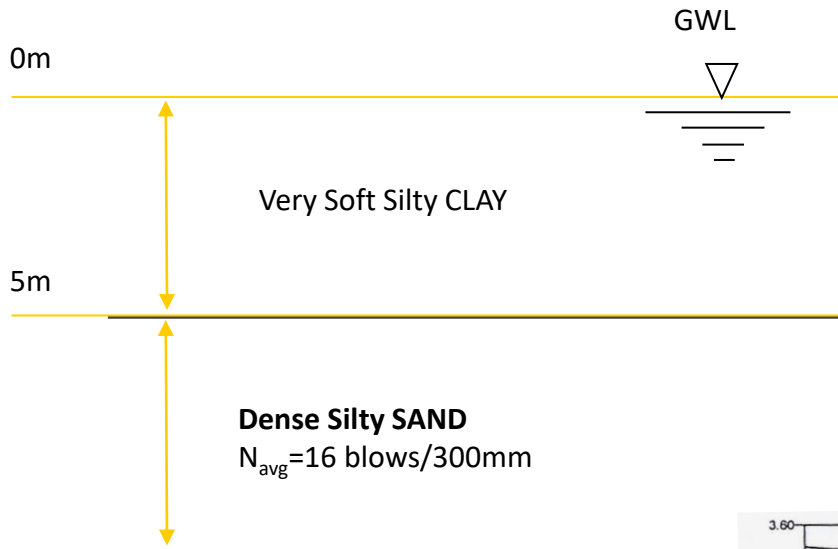
$H$  = length of drainage paths

# Perhitungan muatan surcharge

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1. Calculate  $S_{pf}$  and  $S_{p+q (f)}$  for an assumed  $q$  value
2.  $S_{p+q (t)} = x S_{pf} / 100$
3.  $U_v = S_{p+q (t)} / S_{p+q (final)}$
4. Find  $T_v$  for given  $U_v$
5.  $t_{calc} = T_v H_d^2 / C_v$
6. If  $t_{calc} > t$ ; increase  $q$   
If  $t_{calc} < t$ ; decrease  $q$
7. Repeat calculations until If  $t_{calc} = t$

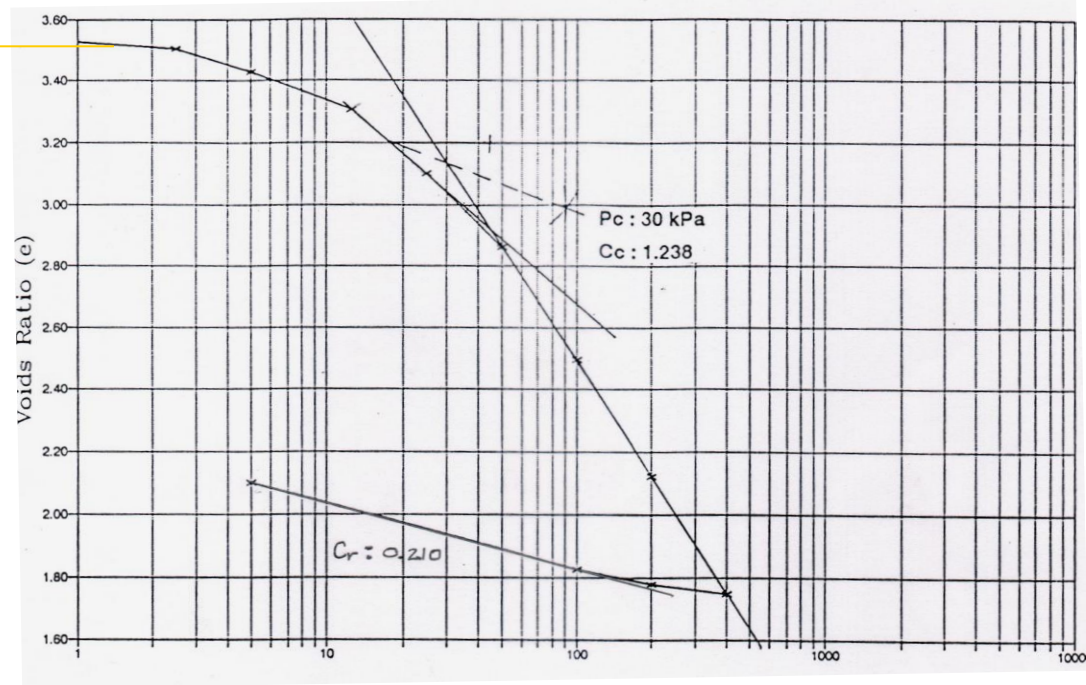


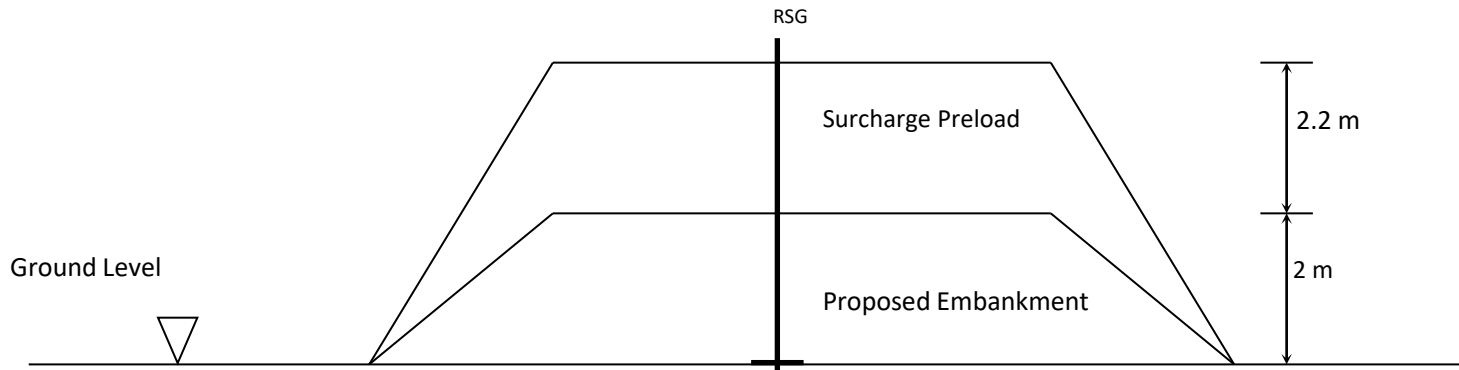


### Very Soft Silty CLAY

$N_{avg}$	=	Hammer Weight
$\gamma$	=	15 kN/m <sup>3</sup>
LL	=	75%
PL	=	42%
PI	=	33%
$P_c$	=	30 kPa
$C_c$	=	1.238
$C_r$	=	0.210
$e_o$	=	3.573
CR	=	0.271
RR	=	0.046
$C_v$	=	2.5 m <sup>2</sup> /yr

## CONTOH SOAL aplikasi





Drainage condition : Two way drainage

**For 2 m embankment:**

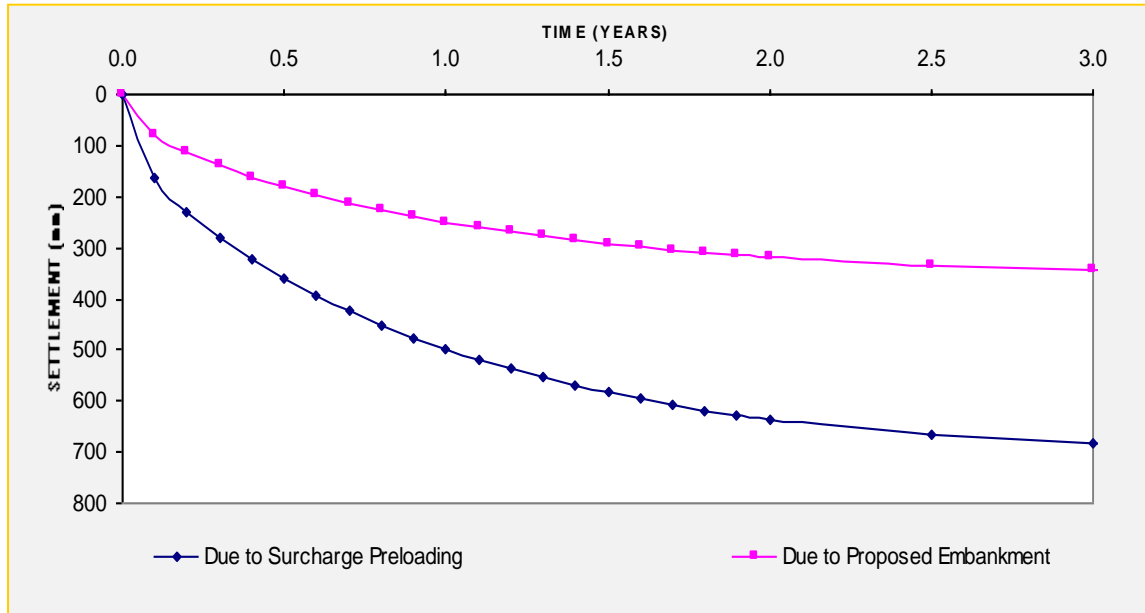
Total settlement = 359.3 mm

Time for 90% Consolidation Settlement = 2.1 years

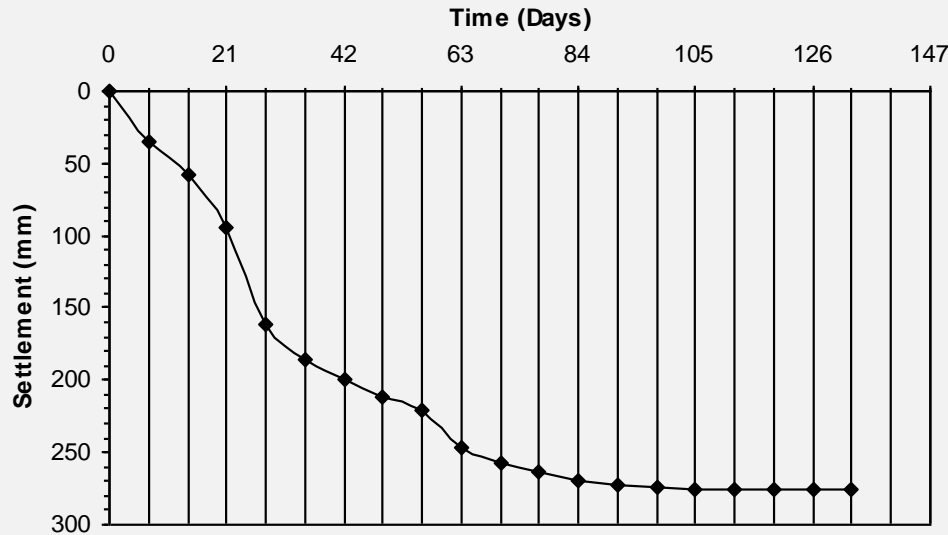
**With 2.2 m surcharge preload:**

Time for total settlement to occur = 0.5 years

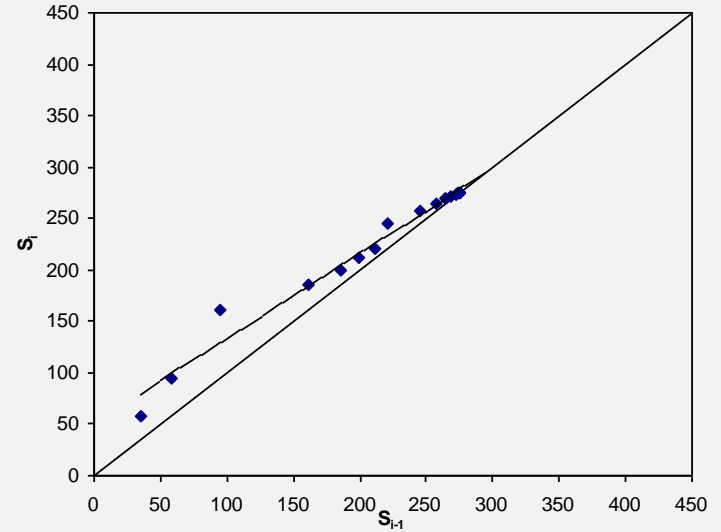
To be scraped off = 1.84 mm



**Settlement vs Time Plot**



**Asaoka's Construction**



Based on the comparisons of estimated and observed settlements, the following conclusion is drawn:

- Most of the settlements completed in 3.4 months.
- the difference between the estimated and observed settlement is about 30%.
- the rate of consolidation was much faster than anticipated.
- the accelerated rate of consolidation may be due primarily to irregular sandy seams within the clay layer. Thus reduces the drainage path distance significantly.

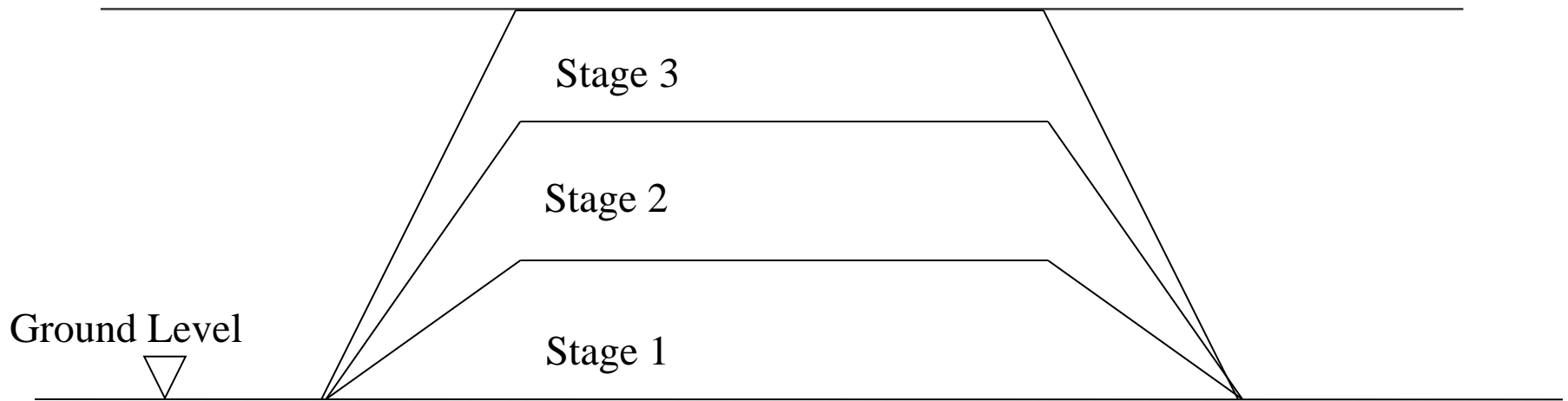
$$m = \tan^{-1} \beta$$

$$C_v = \frac{-5H^2}{12\Delta t} \ln \beta$$

Computed

$$C_v = 11 \text{ m}^2 / \text{yr}$$

# STAGED LOADING

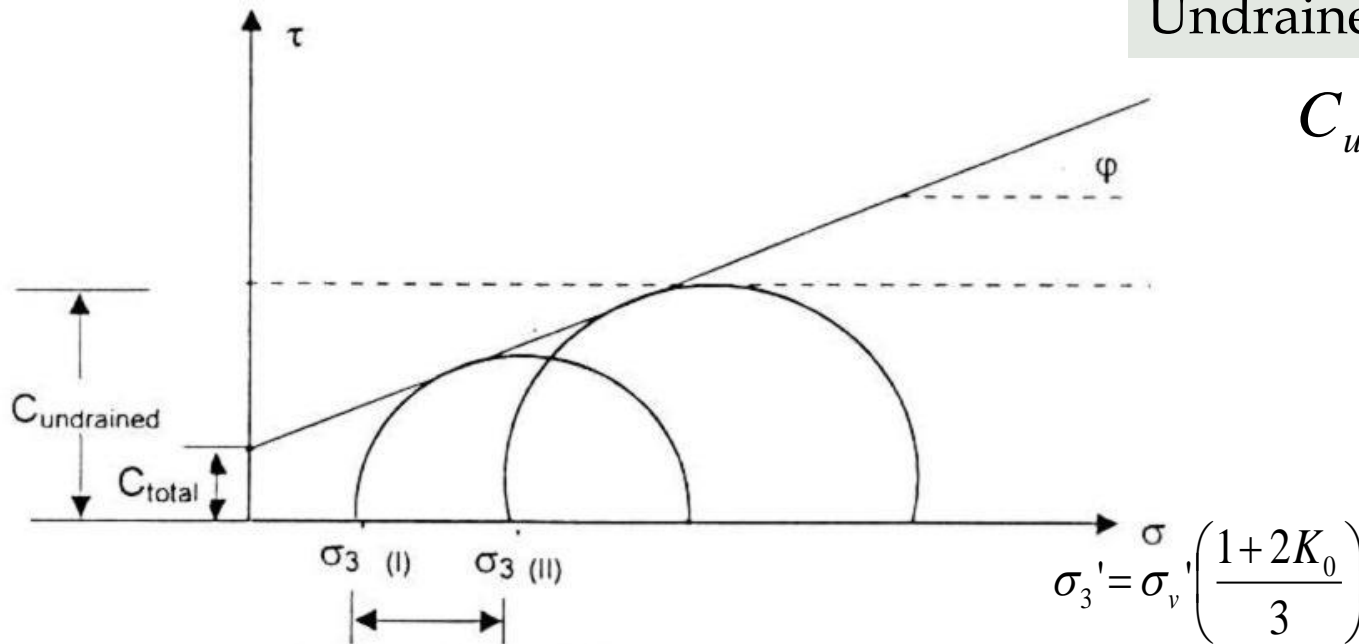


Staged construction may be considered for construction covers large area whereby waiting time could be used for other activities, biggest advantage is **the increase in shear strength.**

# Peningkatan Kekuatan Geser Tanah

From CU Triaxial testing  
Undrained shear strength

$$C_u = (\sigma_1' - \sigma_3') / 2$$



Increase in effective stress

$$\sigma_1' = 2c_u \tan(45 + \phi/2) + \sigma_3' \tan^2(45 + \phi/2)$$

Determination of  $c_u$  from undrained Triaxial testing

# Peningkatan kekuatan geser tanah, Korelasi

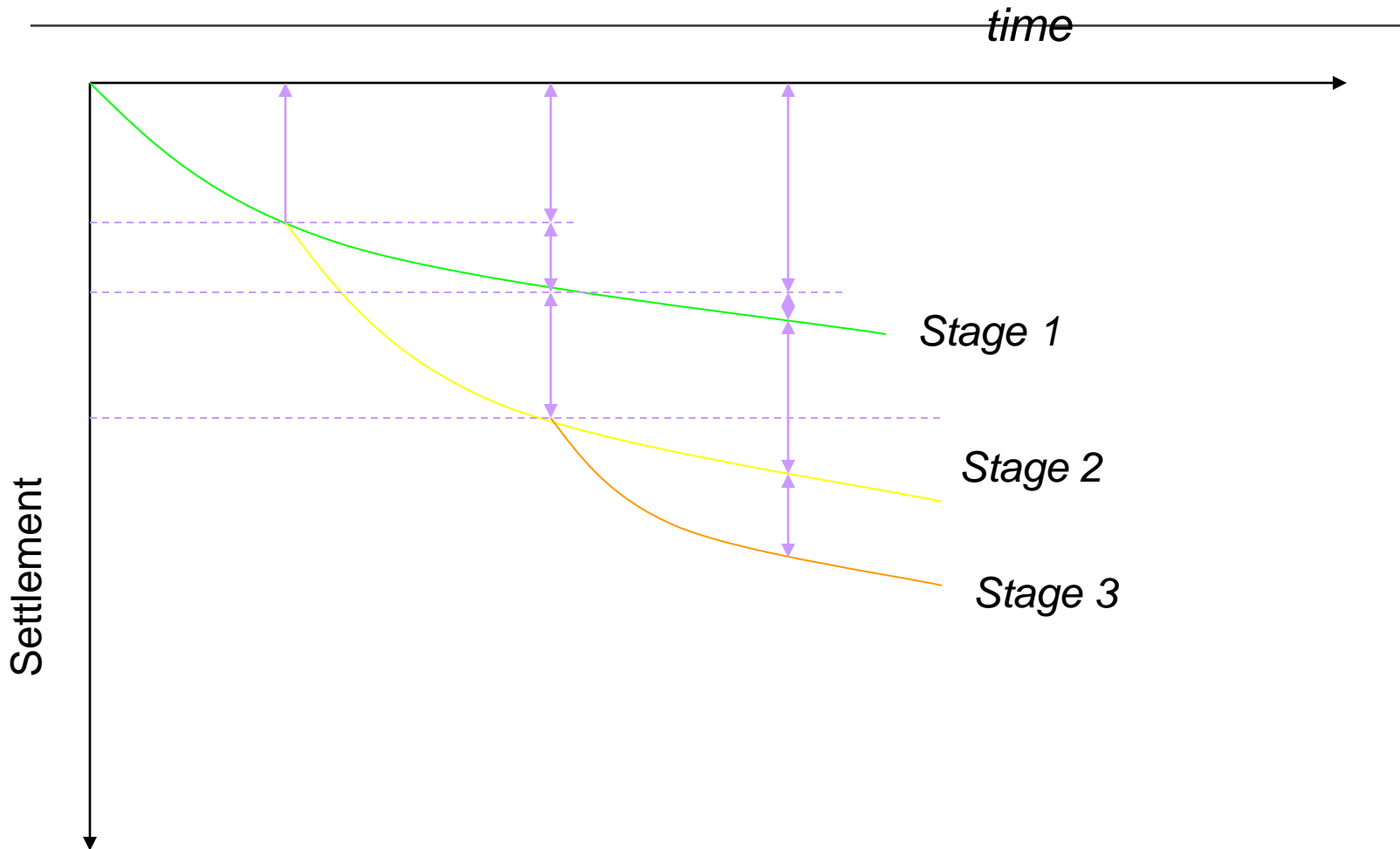
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Empirical correlation Increase in strength due additional overburden pressure after  $U$  90% is reached:

$$(\Delta C_{u/} \sigma'_{o}) = 0.11 + 0.0037 I_p \quad (\text{Skempton})$$

$$(\Delta C_{u/} \Delta \sigma) = 0.22 \quad (\text{Ladd}) \text{ for inorganic clay}$$

# Load-settlement relationship for different $t$



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In staged construction, load can be added at any time, however it is better to wait for 90% consolidation of the previous loading stage. Settlement of each loading stage should be added when calculating the final settlement (**see figure**)

It should be noted that the increase in shear strength only take effect when the consolidation reached almost 100% (take 90%)



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thank you