

# Vertical Drain

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# Preloading + Vertical Drain

Reduces settlement & speeds up primary consolidation

Effective if

- *Soft cohesive soils*
- *Soft clay with horizontal lenses*
- *No or low organic content*
- $C_v < 3 \times 10^{-7} \text{ m}^2/\text{sec.}$

Drainage spacing is determined based on the required time and degree of consolidation

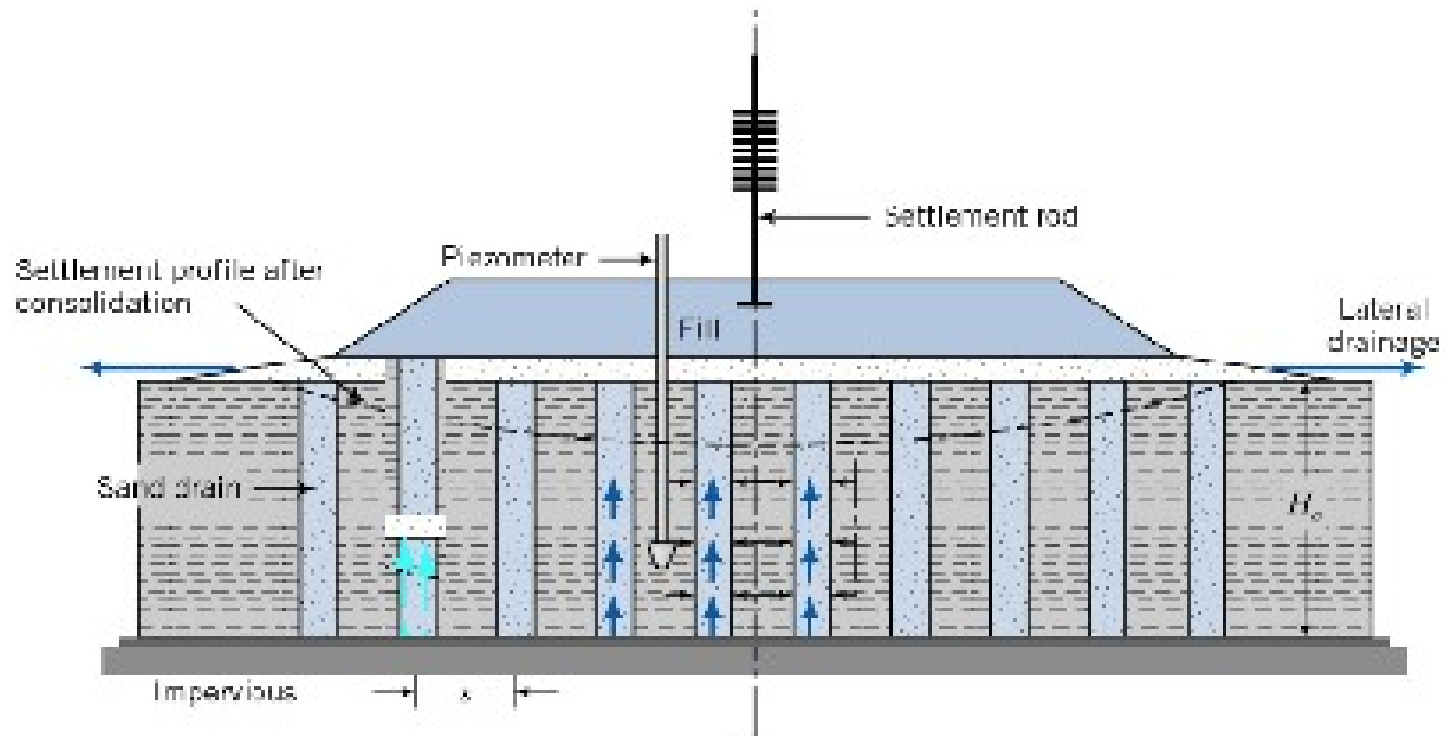
# Methods of Providing Vertical Drain

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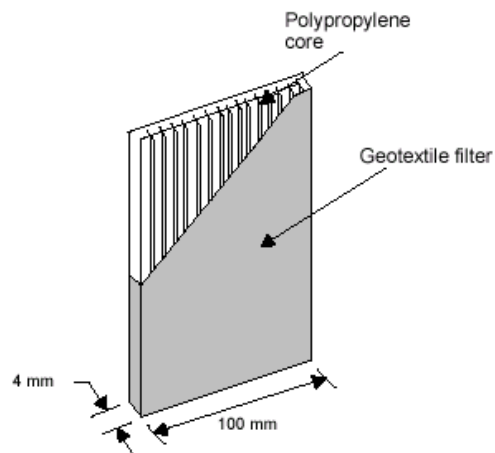
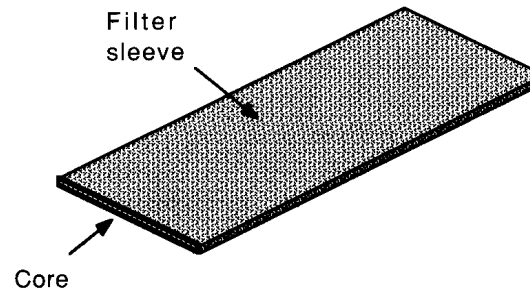
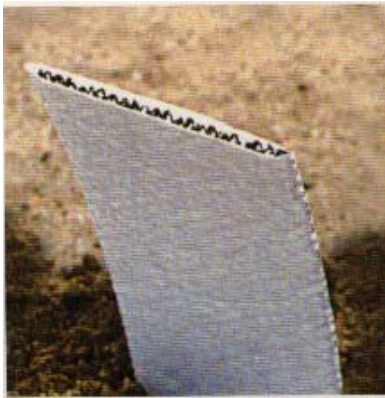
- Sand Drain (typical dia. 200-450 mm, spaced 1.5–6 m)
- Sandwich drains (typical dia. 65 mm)
- Geosynthetics drains (strip drains)

# Sand Drain

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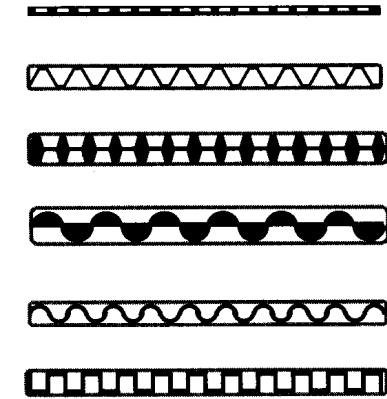


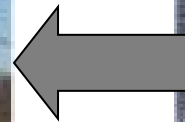
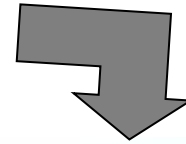
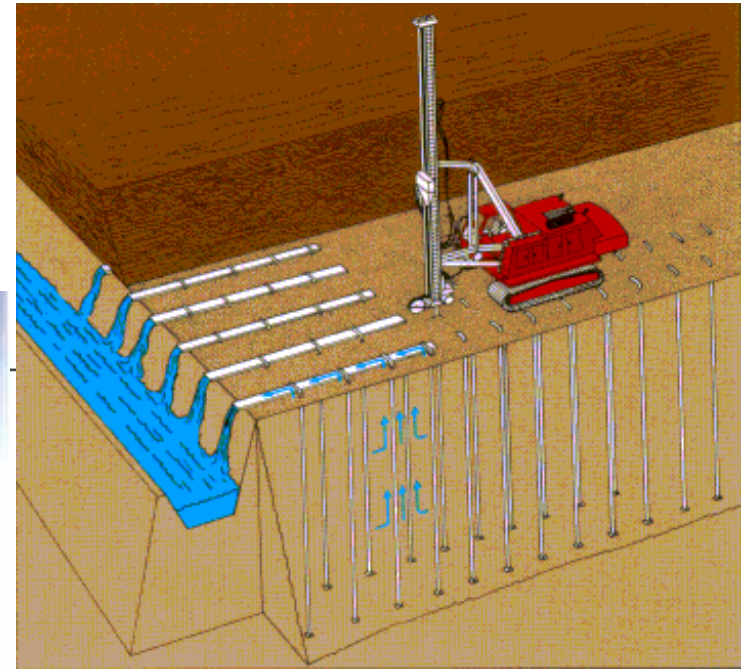
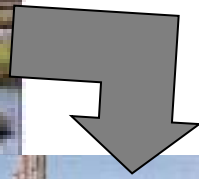
# Prefabricated Vertical Drain / Geosynthetic drain (PVD)



Fluted PVC  
or paper

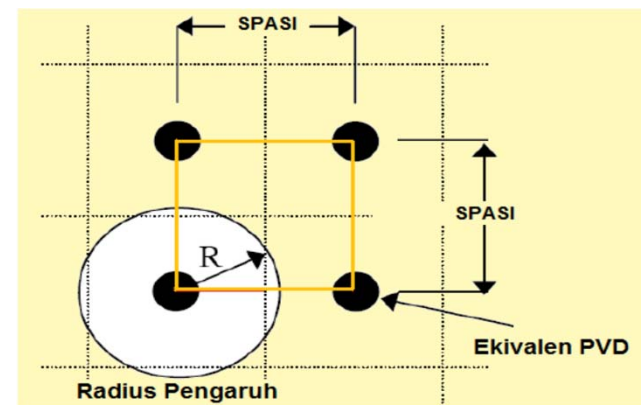
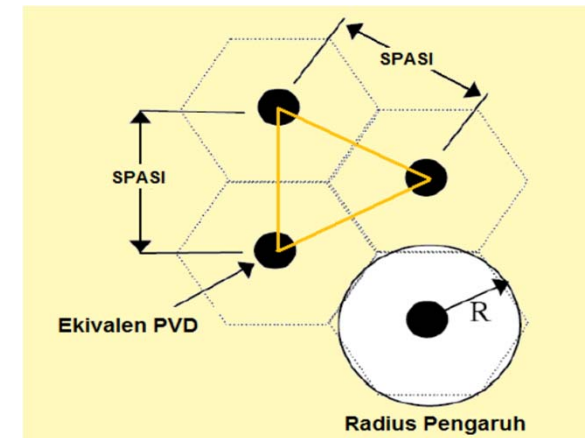
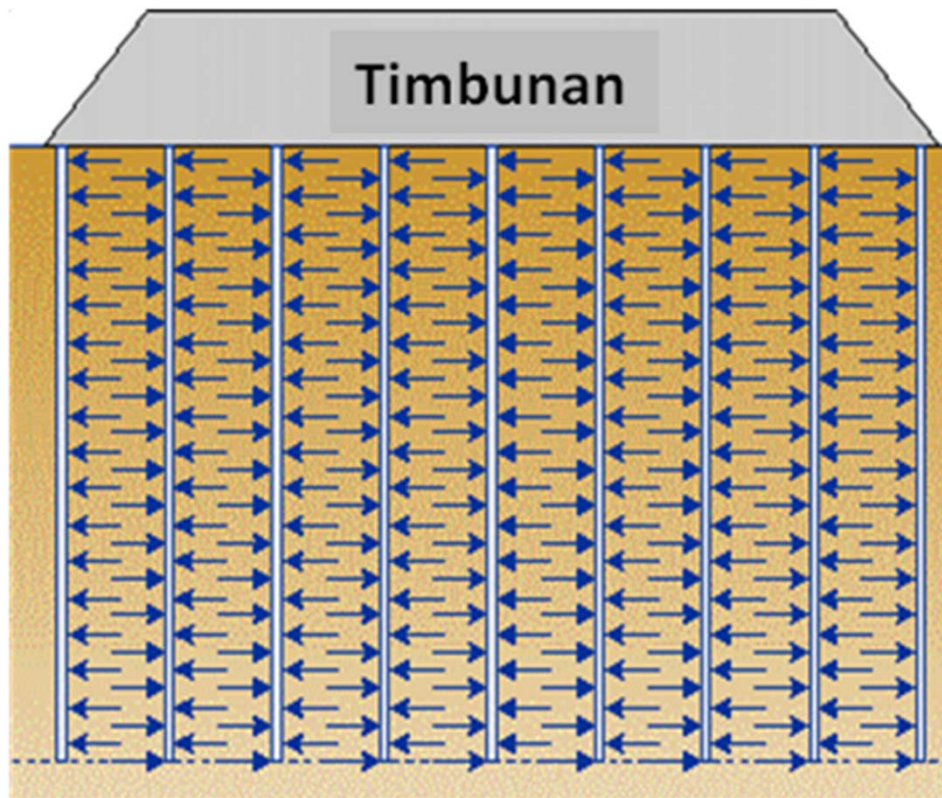
Various shapes  
of cores with  
nonwoven  
geotextile  
filter sleeves







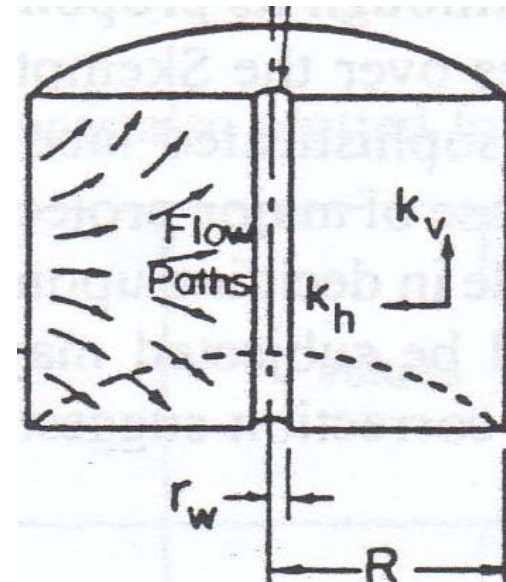
# Vertical drains Prinsip Disain



## Aliran air arah radial

Proses terdisipasinya tekanan eksese air pori pada arah radial diatur melalui persamaan sebagai berikut:

$$\frac{\partial U_e}{\partial t} = C_h \left( \frac{\partial^2 U_e}{\partial r^2} + \frac{1}{r} \frac{\partial U_e}{\partial r} \right)$$





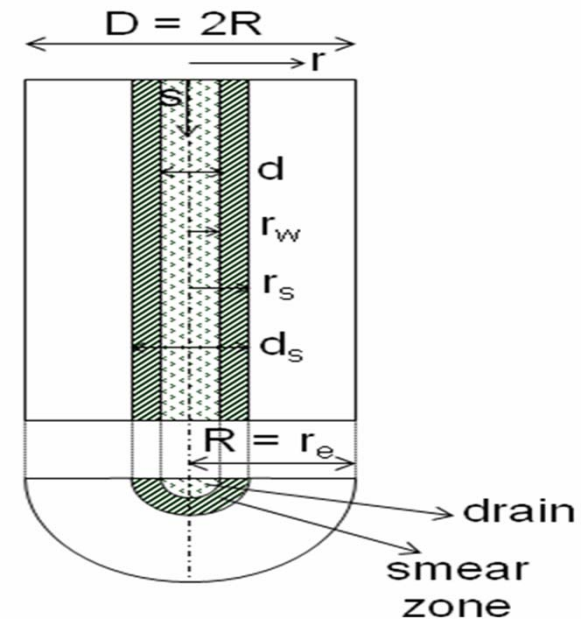
Untuk kasus vertical drain dan dengan asumsi kondisi equal strain, maka solusi dari persamaan di atas adalah:

$$\bar{U}_h = 1 - \exp\left[\frac{-2T_h}{F(n)}\right]$$

dengan

$$T_h = \frac{C_h \cdot t}{r_e^2} \quad n = \frac{r_e}{r_w}$$

$$F(n) = \frac{n^2}{n^2 - 1} \ln(n) - \frac{(3n^2 - 1)}{4n^2} + \frac{k_r}{r_w k} \cdot \frac{n^2 - 1}{n^2}$$

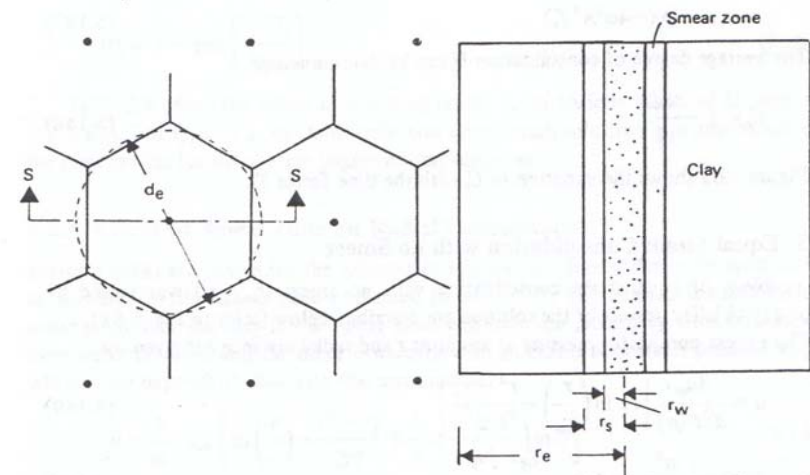
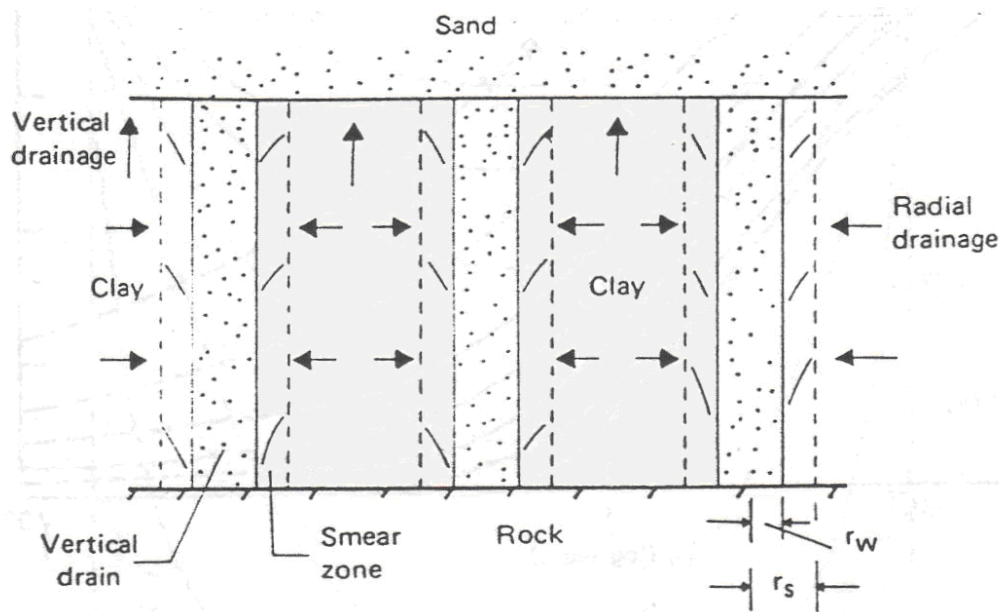


# Aliran air arah vertikal dan arah radial

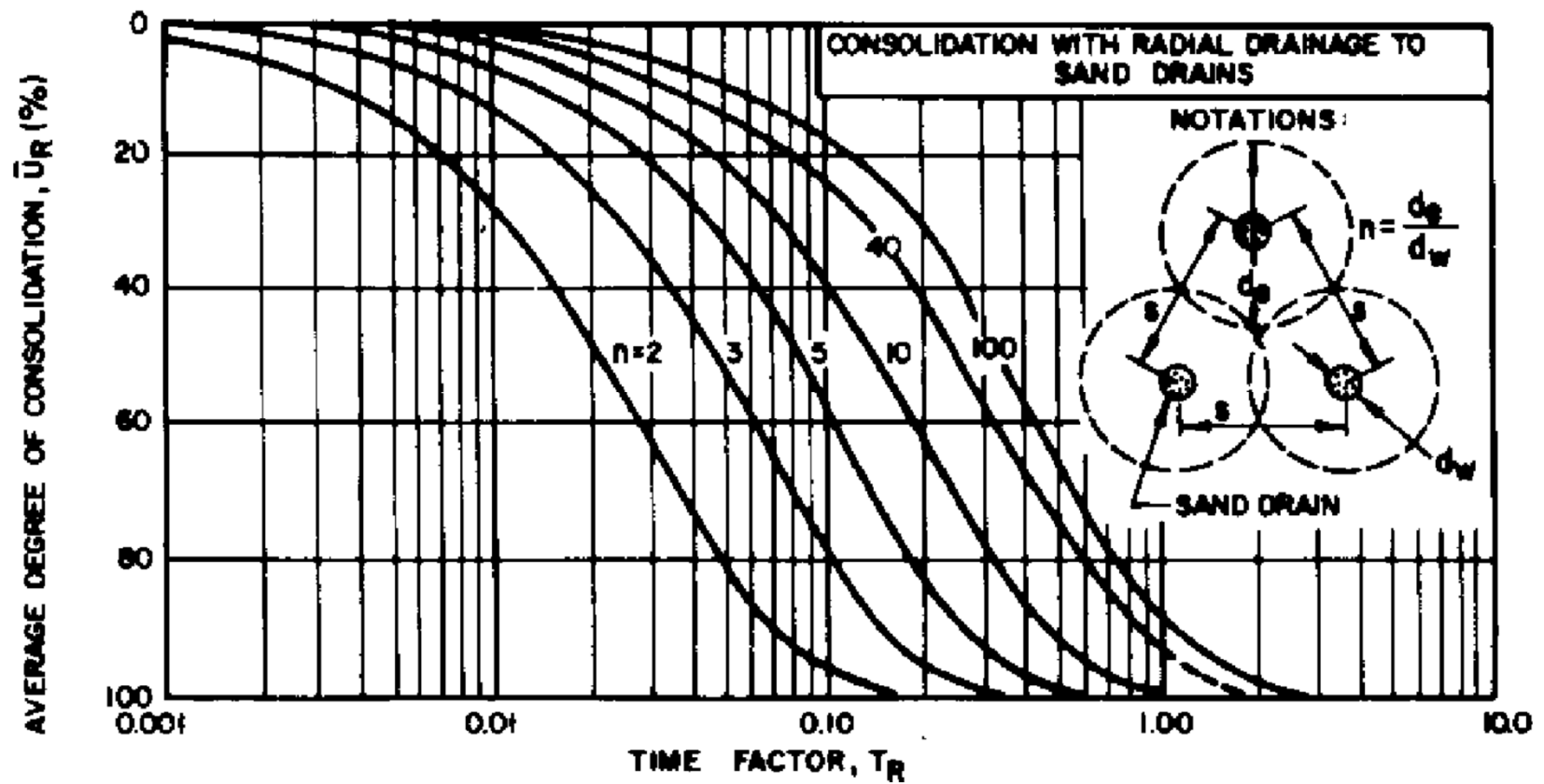
Proses konsolidasi untuk aliran dua arah ini diatur melalui persamaan sebagai berikut:

$$\frac{\partial U_e}{\partial t} = C_v \frac{\partial^2 U_e}{\partial z^2} + C_h \left( \frac{\partial^2 U_e}{\partial r^2} + \frac{1}{r} \frac{\partial U_e}{\partial r} \right)$$

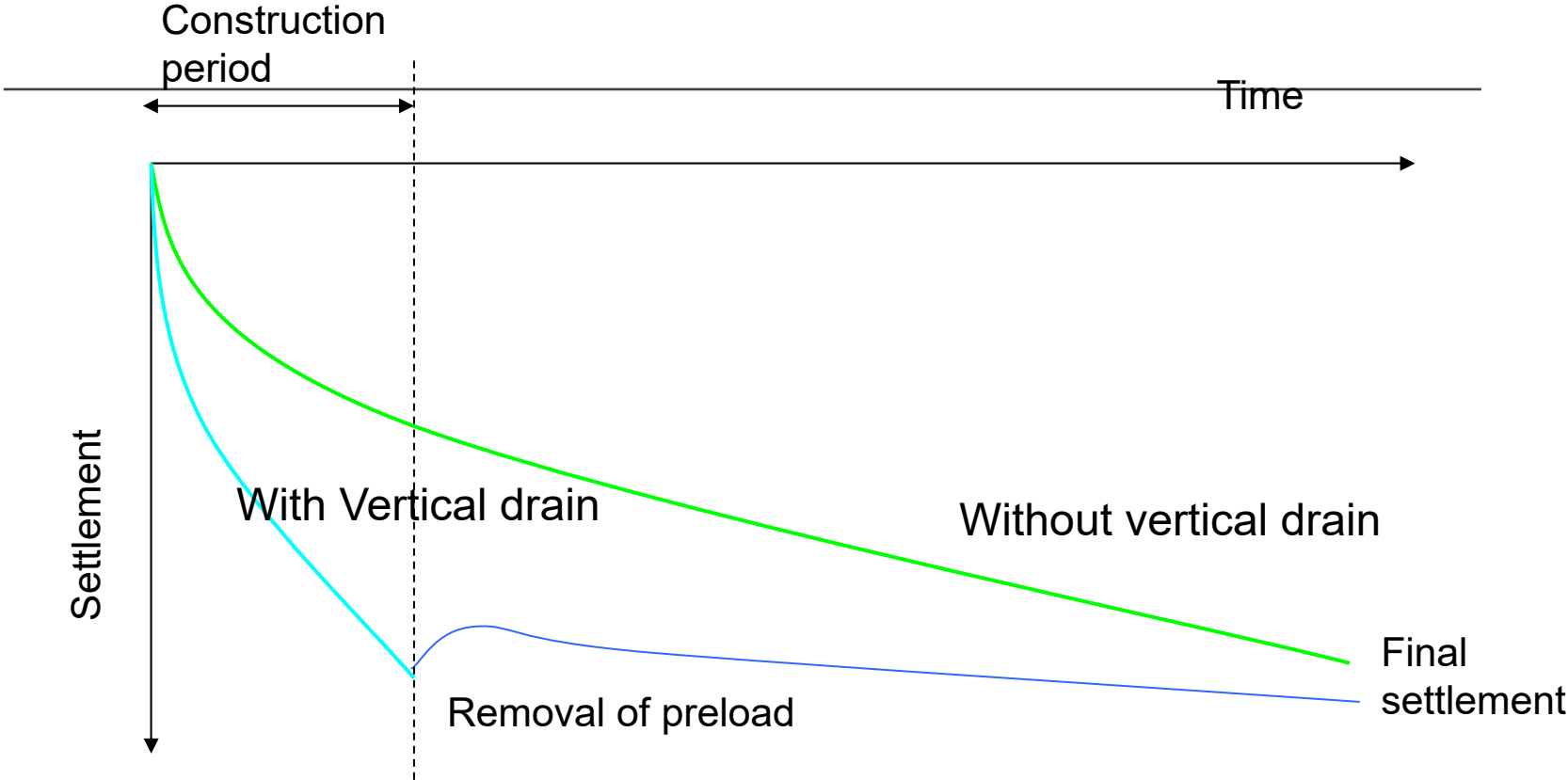
$$\overline{U}_{vh} = 1 - (1 - \overline{U}_v)(1 - \overline{U}_h)$$



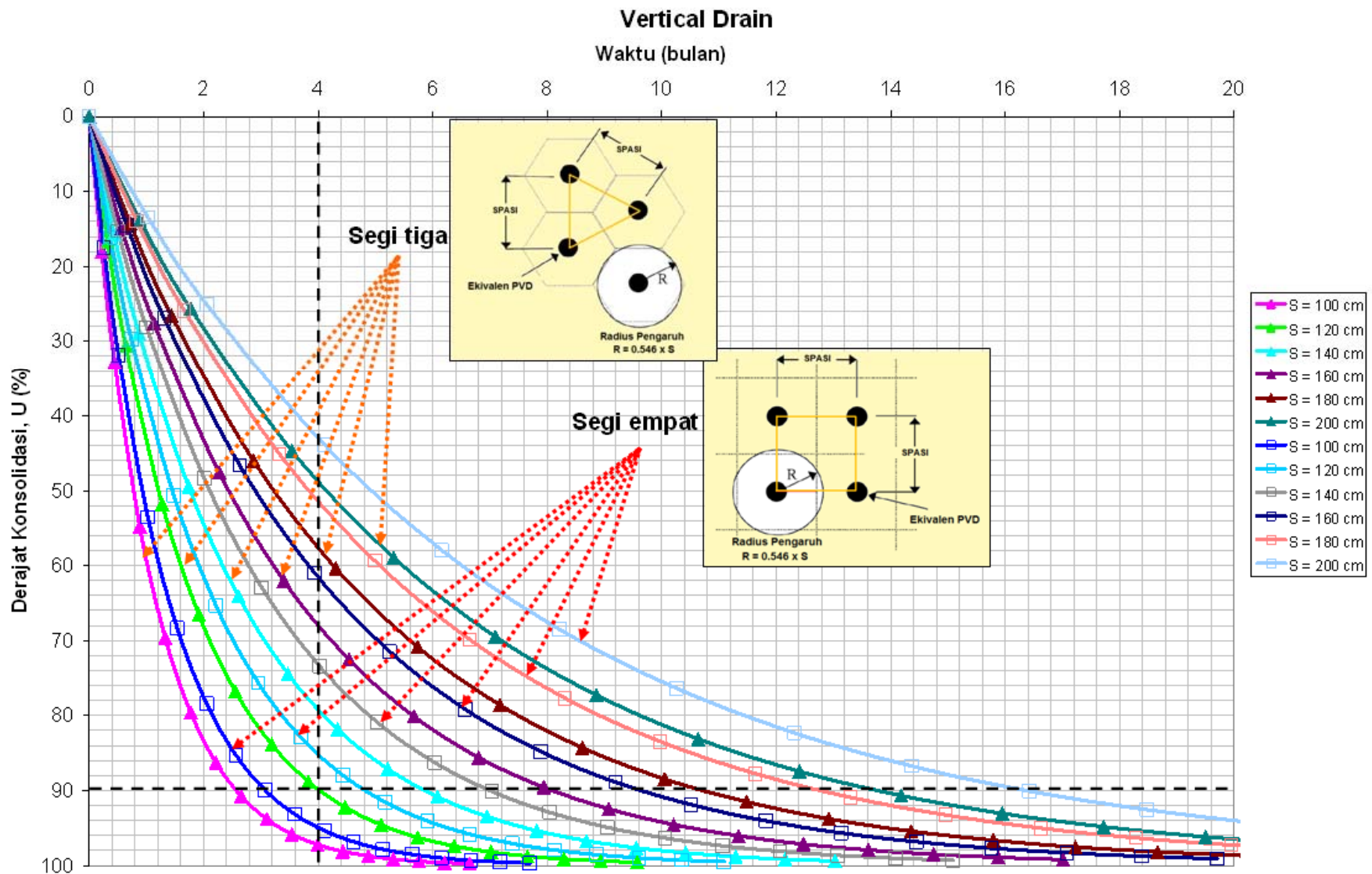
# Radial drain (vertical drain)



# Effect of Vertical Drain on Final Settlement



# Percepatan Proses Konsolidasi dengan PVD



# Effect of Smear & Drain Resistance on vertical drain

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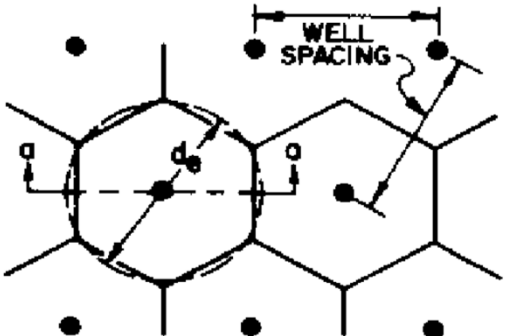
**Smear** is the disturbance of the soil adjacent to the drains that can decrease the permeability and slow down the consolidation process

**Smear effect increases with increasing drain diameter**

Dynamic driving creates more disturbance than the static driving

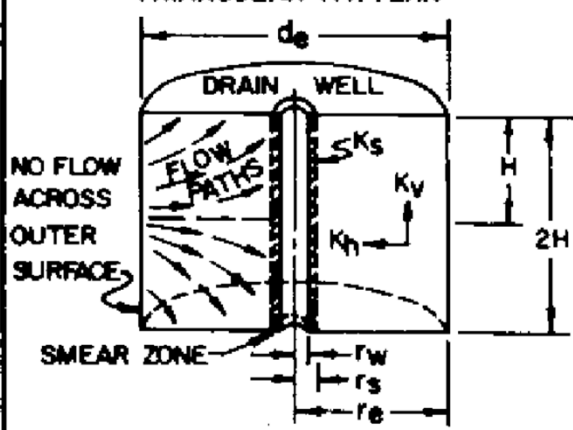


# Radial drain (vertical drain) with smear



WELL SPACING

DRAIN WELLS IN TRIANGULAR PATTERN



SECTION a-a

**DEFINITIONS**

FOR TRIANGULAR PATTERN  
 $d_e = 1.05$  (WELL SPACING)

FOR SQUARE PATTERN  
 $d_e = 1.14$  (WELL SPACING)

$d_e$  = EFFECTIVE DIAMETER OF SAND DRAIN.

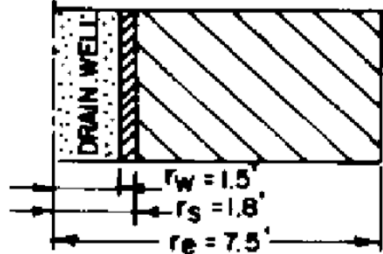
$K_h$  = HORIZONTAL PERMEABILITY  
 $K_s$  = SMEAR ZONE PERMEABILITY

$n = \frac{d_e}{d_w} = \frac{r_e}{r_w}$   
 = EFFECTIVE RADIUS / RADIUS OF DRAIN

$s = \frac{r_s}{r_w}$   
 = RADIUS OF SMEAR ZONE / RADIUS OF DRAIN

**EXAMPLE: TO DETERMINE EQUIVALENT RADIUS OF DRAIN WITHOUT SMEAR WHOSE EFFECT IS EQUAL TO THE ACTUAL DRAIN WITH SMEAR.**

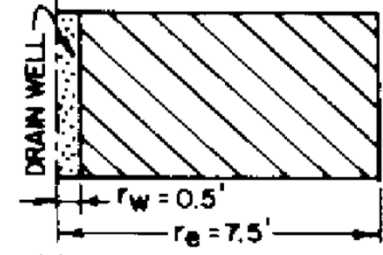
GIVEN:



ACTUAL SAND DRAIN  
 $n = 5, K_h/K_s = 7$   
 ESTIMATED  $S = 1.2$

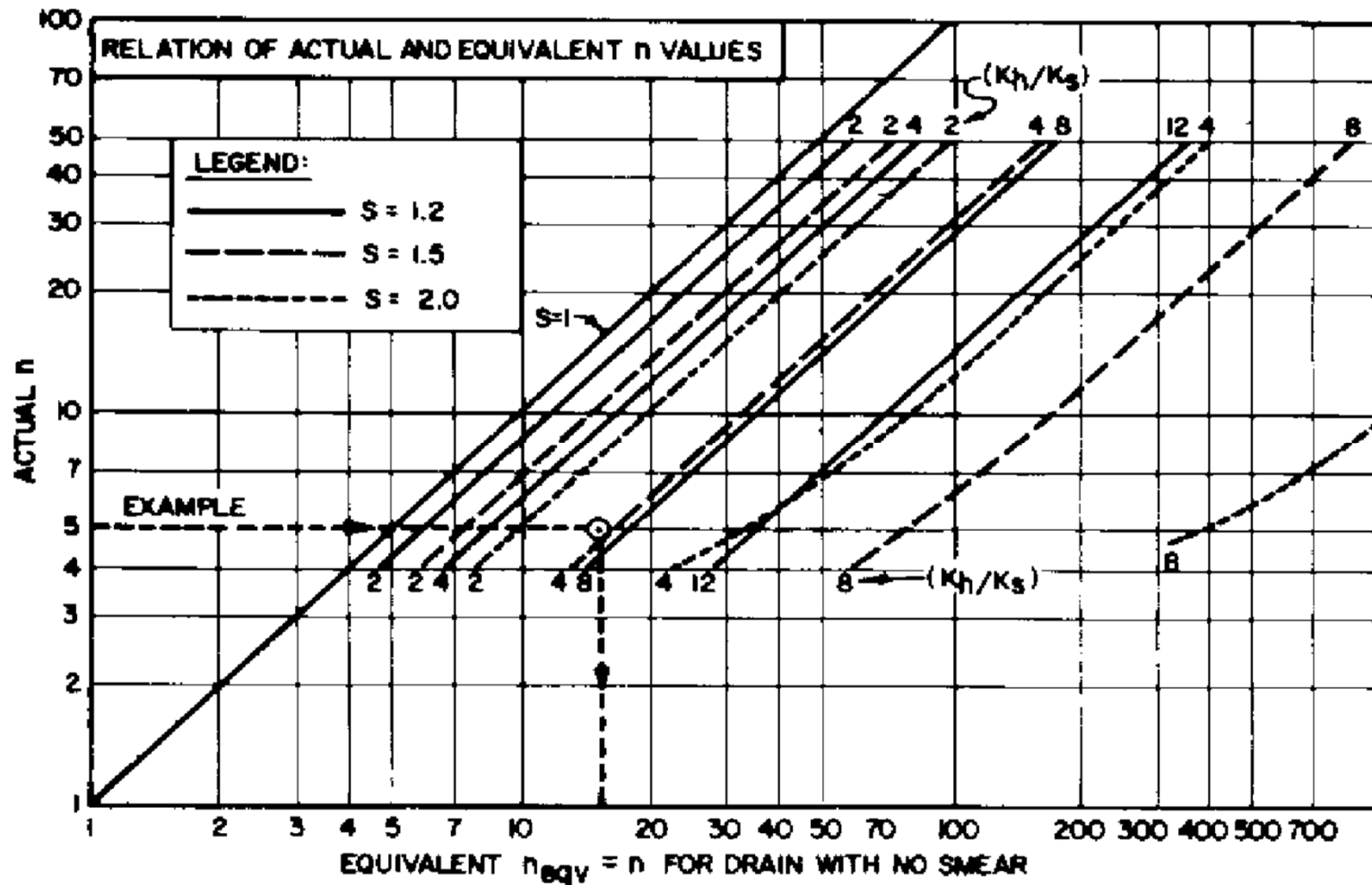
DETERMINE  $n_{eqv}$  FROM DIAGRAM ABOVE:

$n_{eqv} = 15, r_w = \frac{7.5}{15} = 0.5'$



EQUIVALENT SAND DRAIN, NO SMEAR

# Radial drain (vertical drain) with smear



# Contoh Kasus : Perbandingan antara Prediksi dan Hasil Monitoring Penurunan PVD Treated Railway Embankment

CONSTRUCTION OF RAILWAY EMBANKMENT  
REQUIRES STRINGENT POST CONSTRUCTION  
SETTLEMENT CRITERIA

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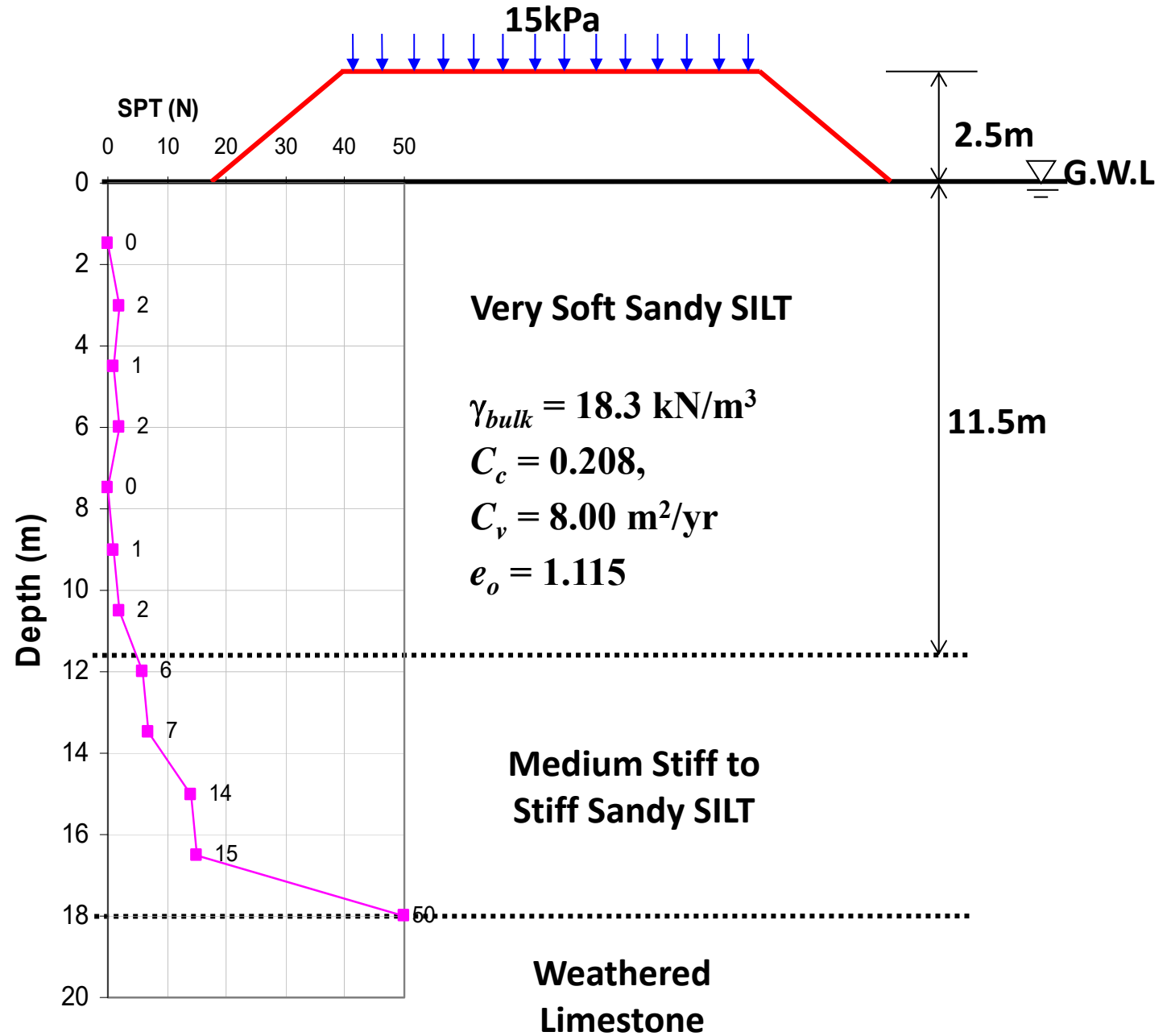
SPECIFIC DESIGN CRITERIA BY KTMB :

# Background and Client Requirement

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1. Maximum settlement of 25mm over 6 months of commercial service
2. Maximum differential settlement of 10mm for a chord of 10m over 6 months of commercial service
3. Additional criteria for preloading/surcharging (for planning purpose) : Maximum time for any preloading/surcharging = 3 months

# Soil Profile



## Calculation of the Consolidation Settlement

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Consolidation Settlement was calculated using the following equation (based on Terzaghi's 1-D theory) :

$$S = H \cdot \frac{C_c}{1 + e_0} \cdot \log \left( \frac{P_o' + \Delta P'}{P_o'} \right)$$



**For PVD design, the following formula was adopted to calculate % of consolidation,  $U_h$  (based on Hansbo, 1979) :**

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$$U_h = 1 - \exp\left(\frac{-8C_h t}{D^2 \mu}\right)$$

**where:**

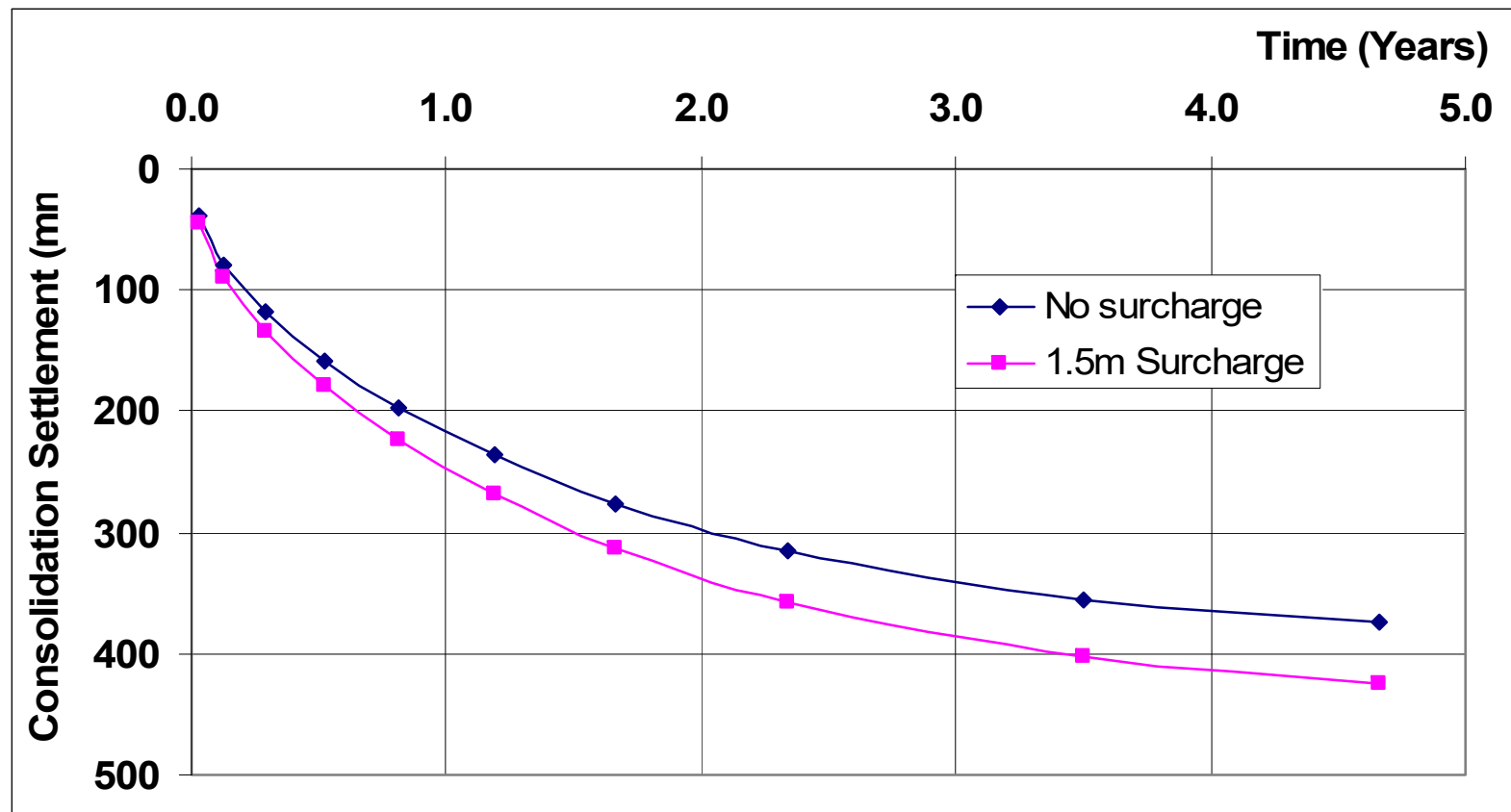
$$\mu = \ln(n) - 0.75, \quad n = D/d, \quad d = 2(b+t)/\pi,$$

$$D, \text{ Dia. of dewatered cylinder} = 1.05S \text{ (triangular grid)} \\ = 1.13S \text{ (square grid)}$$

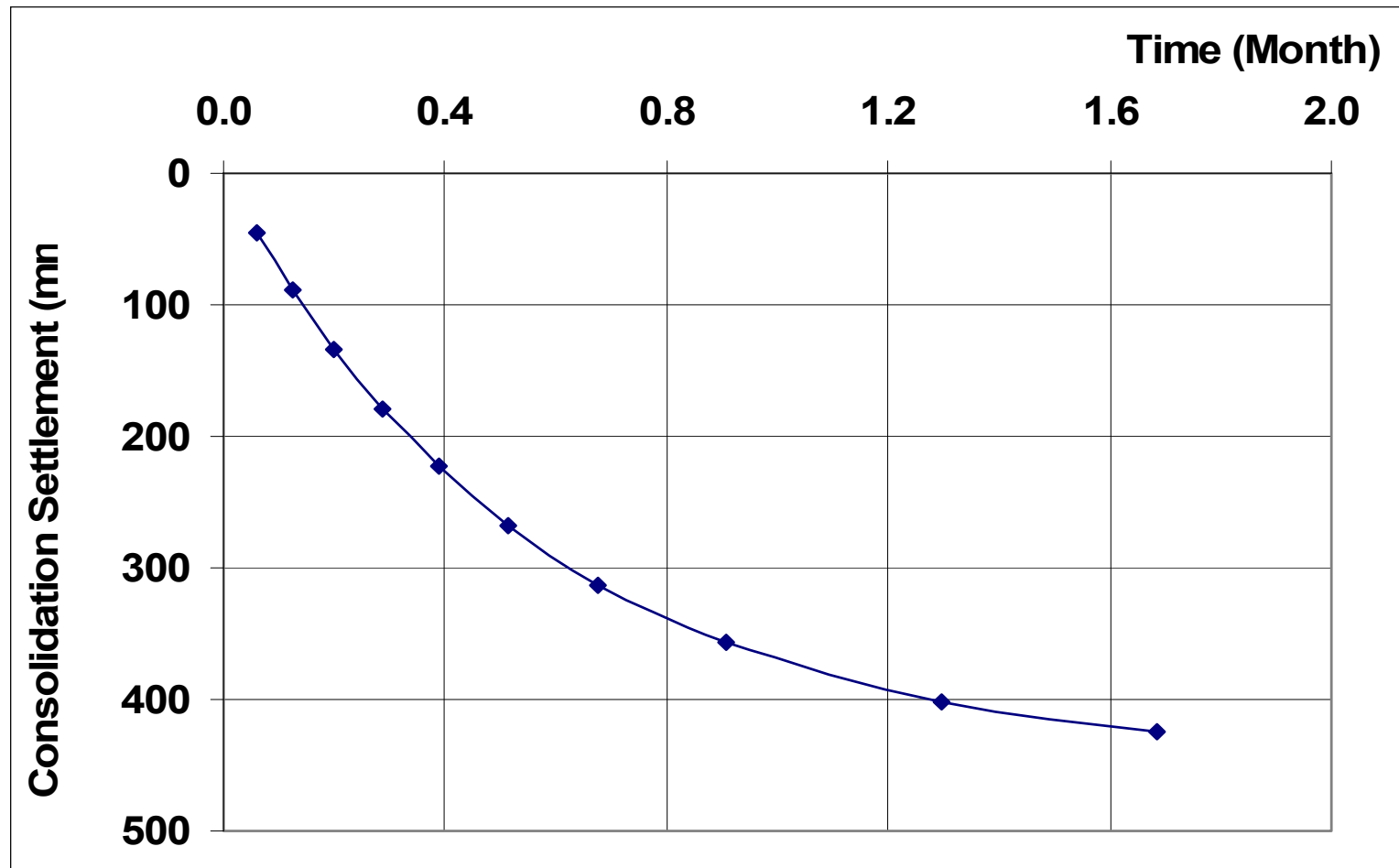
**$C_h$  = Coeff. Of Consol. in horizontal pore water flow**

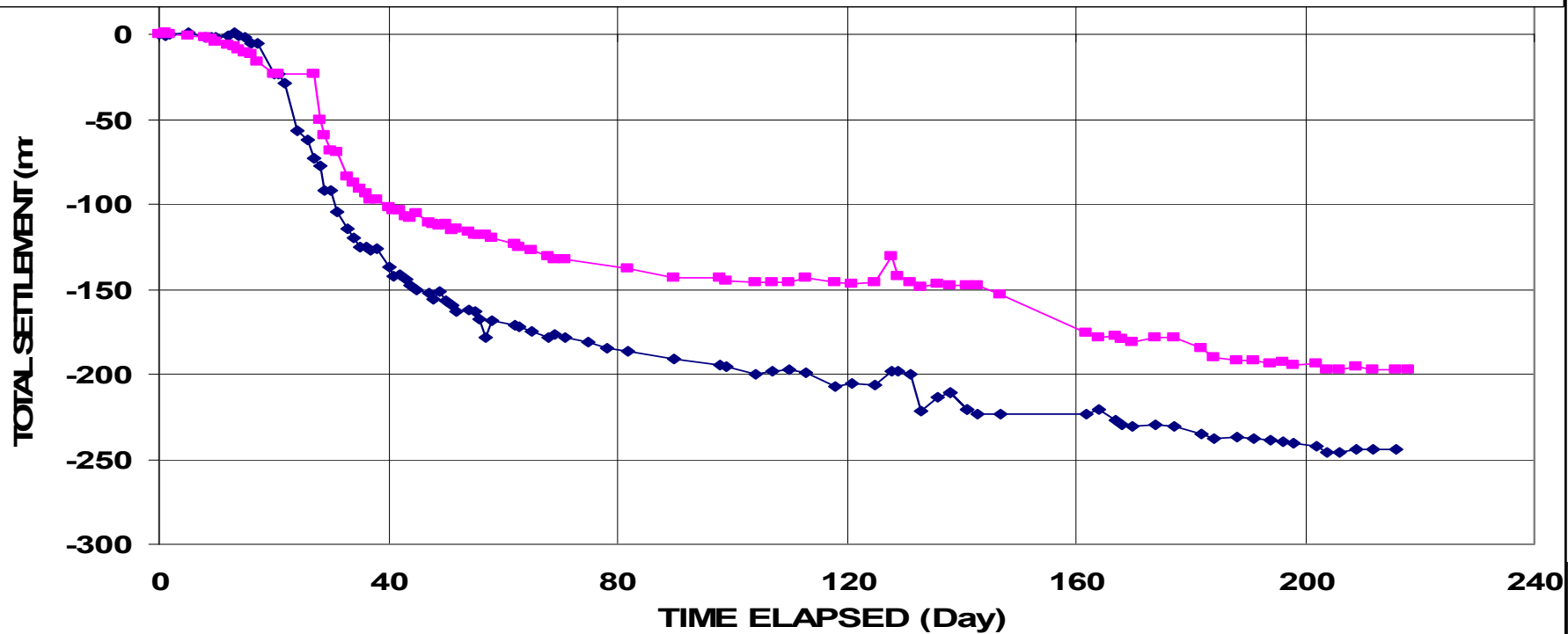
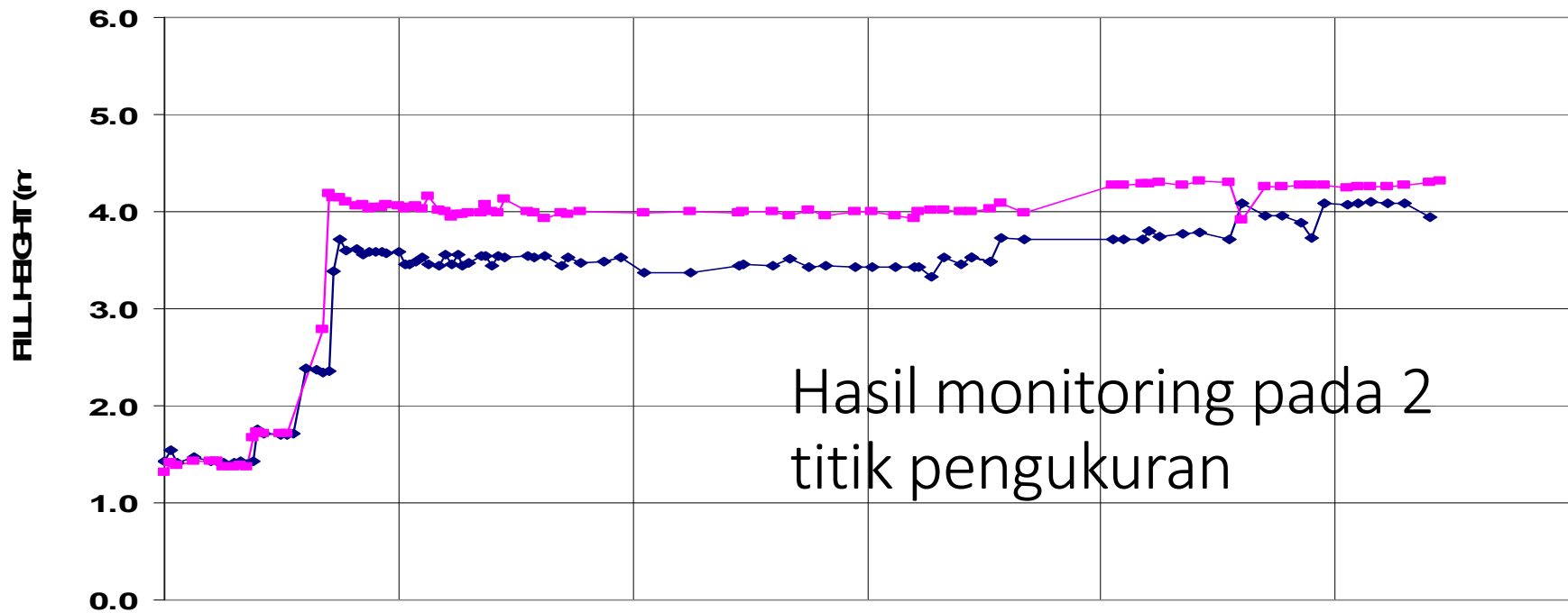


# Predicted Consolidation Settlement vs Time for Embankment with/without Surcharge



## Predicted Consolidation Settlement vs Time for Embankment with PVD + Surcharge





- Comparison between the design and back-calculated settlement parameters are tabulated as below :

Parameter	$\frac{C_c}{1+e_o}$	$C_h$ (m <sup>2</sup> /yr)
Design	0.10	16.0
Back-calculated	0.06	9.5

- The estimated settlement was comparable to the recorded settlement. However, the rate of settlement recorded was slower than the prediction.
- Percentage of dissipation of  $\Delta u$  is not known due to the absence of piezometer, but can be reasonably estimated with the settlement plate record & settlement markers.

**Thank you ...**

